

HERMES DECLARATION EXHIBIT 7 – PART 1 OF 2

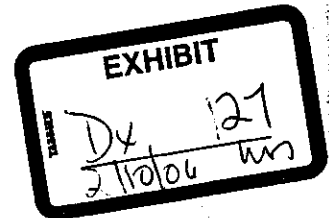
BOOK NO. 2175

ETHICON, INC.
a Johnson & Johnson company

Issued to Mark Stuckel

Covering the Period

Feb 29, 1988 to _____



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DePuy Mitek, Inc. v. Arthrex, Inc.

C.A. No. 04-12457 PBS

DMI002605

This Page Is Reserved for
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Book No.

Project No. 16211 - STS Experiment No. Date 3/31/88
 Subject STS - PTFE BRAIDS - REPLICATION OF A. HUNTER'S STS CONSTRUCTIONS
 Purpose TO VERIFY THE MANUFACTURING CONDITIONS FOR THREE

2175

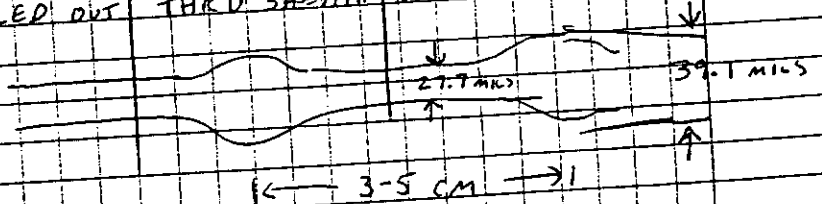
STS BRAID CONSTRUCTIONS (SIZE 2/0, 0, 2) WHICH WERE
 DEVELOPED BY A. HUNTER.

NOTEBOOK #	2175-1A	2175-1B	2175-1C
EXPERIM. # (O. REMBERT)	STZ-001	STZ-002	STZ-003
START DATE	3/28/88	3/28/88	3/28/88
BRAIDER #	1	00	3
SIZE	2	0	2-0
YIN COLOR/DEK	PTFE / WHITE	PTFE / WHITE	PTFE / WHITE
CONSTRUCTION	16 x 3	12 x 1	8 x 1
PULL GEAR	40	31	42
BRAIDER RPM	100	400 (9 YDS/HR)	9 YDS/HR
SHEATH LOT #	225-30-0-TIMS	225-30-0 TIMS	225-30-0 TI 143
SHEATH CONSTR.	1/0 225 DEN DuPont	225 DEN x 1/0	225 DEN x 1/0
SHEATH DESCRIP	PTFE MULTIFIL	PTFE MULTI (DuPont)	PTFE MULTIF. (DuPont)
CORE DESCRIP	PTFE MULTIF. (DuPont)	PTFE MULTI (DuPont)	PTFE MULTIF. (DuPont)
CORE LOT #	225-30-0 TIMS	225-30-0 TI 143	225-30-0 TI 143
CORE CONSTR.	1/3 450 DEN	1/0 225 DEN	225 DEN x 1/0
SHEATH TENSION SPRING	0.011 x 5 1/2 GRN	0.009 x 5" NAT	0.009 x 5" NAT
CORE TENSION SPRING	0.011 x 5 1/2 GRN	0.009 x 5" NAT	0.009 x 5" NAT
TEN DEN (CORE)	BUTT CARRIER	BUTT CARRIER	BUTT CARRIER
QUANTITY	480 YDS	500 YDS	760 YDS

COMMENTS:

2175-1A: RANDOM MODULAR GEOMETRY VISIBLE WITH NAKED
 EYE AT 3-5 CM INTERVALS APPARENTLY
 DUE TO "CORE-POPPING" (CORE CAN BE
 PULLED OUT THRU SHEATH WALL AT NODE).

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MICRO EVAL (25X): A GREAT DEAL OF ENTRAPPED
 BLACK CONTAMINANT, V. LITTLE BROKEN
 FILAMENTS

Investigator
 Witness

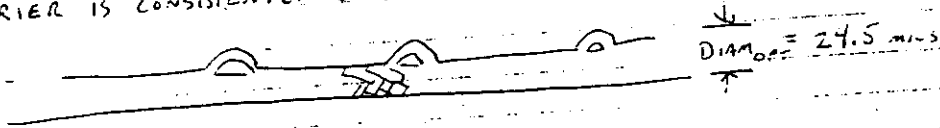
Michael Stahel
Christopher Britt

Date 4/14/88
 Date 3-15-90

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Project No. (CONT.) FROM PREVIOUS PAGE Experiment No. _____ Date _____
 Subject _____
 Purpose _____

2175-1B: VISUAL BUMPY SURFACE. MICRO EVAL (25X) - ONE
 CARRIER IS CONSISTENTLY BUCKLED OUT OF BRAID STRUCTURE.



2175-1C: VISUAL - SLIGHTLY IRREGULAR SURFACE.
 MICRO EVAL (25X) - BRAID SOMEWHAT LOOSE -
 ESPECIALLY ONE OR TWO CARRIERS WHICH OCCASIONALLY
 SLIGHTLY BUCKLE OUT OF PLANE. BRAID APPEARS
 FACETED DUE TO 8 CARRIER CONSTRUCTION.
 ORTIL DIAM: 17.0 mil

GENERAL OVERALL COMMENTS: BRAID PROCESS CONDITIONS
 REQUIRE OPTIMIZATION.

3/31/93 MS

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DMI002608

Investigator

Witness

[Signature]
 Conrad Aritt

Date

Date

3/16/90

3-15-90

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Book No.

2175

Project No. 16211-ST5 Experiment No.

Date 3/31/89

Subject PROCESS CHANGES FOR ST5 BRAIDS

Purpose TO OBTAIN HIGHER QUALITY BRAID STOCK FOR ST5 SIZES 2, 2/0, AND 0 BY ADJUSTING CARRIER TENSIONS ON BRAIDER. PREVIOUS PROCESS CONDITIONS REPORTED BY A. HUNTER RESULTED IN CORE-POPPING AND OTHER BRAID DEFECTS (2175-1A, 1B, 1C).

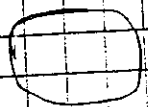
NOTE: ALL BRAID PROCESS CONDITIONS SAME AS 2175-1A, 1B AND 1C EXCEPT FOR:

NOTEBOOK #	2175-3A	2175-3B	2175-3C
EXPER #	STZ-004	STZ-005	STZ-006
START DATE	3/31/88	3/31/88	3/31/88
SHEATH TENSION SPRING	0.011 x 5 1/2 GN	0.009 x 5 NAT	0.009 x 5" NAT
CORE TENSION SPRING	0.012 x 5 1/2 OR	0.011 x 5 1/2 GN	0.011 x 5 1/2 GN
OTHER CHANGES		ONE CARRIER REMOVED AND CLEANED (TENSION: MECH STICKING), CHANGE ALL SPRINGS, 3 BOBBINS CHANGED	NEW SPRINGS, CHANGE 4 CARRIERS, CLEAN BRAIDER

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Comments:

2175-3A: HIGHER CORE TENSION ELIMINATED CORE-POPPING OBSERVED IN 2175-1A. GOOD QUALITY (25X), GOOD CIRCULAR GEOM. SOME TRASH. OPTICAL DIAM - 27.1 MIL.

2175-3B: GOOD QUALITY, SMOOTH. MICRO EVAL (25X): SOME OCCASIONAL LOOSENESS AND BROKEN FILAMENTS. BRAID SOMEWHAT RECTANGULAR IN X-SECT:  IMPROVEMENTS PROBABLY DUE TO CARRIER CHANGES + CLEANING

2175-3C: IRREG SMOOTHNESS. 25.2 MIL. GOOD QUALITY BUT SQUARISH X-SECT DUE TO PACKING CHAR OF 8 CARRIER CONSTRUCTION. WITH THIS YARN. OPTICAL DIAM: 17.6 MILS

Investigator

Witness

Date

Date

3/31/88

3-15-90

DePuy Mitek, Inc. v. Arthrex, Inc.

C.A. No. 04-12457 PBS

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Book No.

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Project No. 16211-ST4 Experiment No. Date 4/15/88
 Subject DIE-DRAWING TRIALS OF STS PTFE BRAIDS / INCOMING YARN VARIABILITY
 Purpose:

PROCEDURE: DIE-DRAWING OF PTFE BRAIDS PERFORMED PER AL HUNTER'S "PROCESS TRANSFER MEMO OF STS SUTURES" OF 10/29/87, SUCH AS (1) BRAID WAS DRAWN THRU STEEL WING DIES, (2) BRAID WAS SIMULTANEOUSLY BEING HOT-STRETCHED USING GODDET SET-UP AND A FORCED CONVECTION TUNNEL OVER AT 3150F, AND (3) MULTIPLE PASSES WITH DECREASING DIE SIZE.

RESULTS

- DIE-DRAWING SIGNIFICANTLY REDUCES THE BRAID PROFILE OF THE PTFE BRAIDS IN ALL CASES IN THE "UNPERTURBED" OR RELAXED CONDITION. HOWEVER, A LOW AMOUNT OF TENSION OR EVEN BENDING OF THE SUTURE TYPICAL OF THE MANIPULATION REQUIRED FOR KNOT TIE-DOWN RESULTS IN A DRASTIC OPENING UP OF THE BRAID STRUCTURE. THUS, THE BRAID STRUCTURE IS APPARENT IN USE ALTHOUGH IT APPEARS 'MONDPELLANT-LIKE' IN THE RELAXED CONDITION.
- PRODUCT UNIFORMITY (DIAMETER) IS CRITICAL IN THE DIE-DRAWING OPERATION WITH THE RISKS OF FREQUENT LINE BREAKAGE ^{OVERSIZED} (LARGE REGIONS) AND ROUGH (UNDERSIZED REGIONS) FOR VARIABLE MATERIAL. THIS MOST LIKELY RESULTS FROM THE APPARENT LARGE VARIATIONS IN YARN DENIER (AND DIAMETER) OF THE DUPONT TEFLON YARN. TYPICAL DEVIATIONS WERE:

DUPONT LABELED

DEN

66

64

84

ETHILON

MEAS. DEN.

88

83

102

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C.A. No. 04-12457 PBS

DMI002610

Investigator

Witness

Patricia Britt

Date

Date

4/15/88

3-15-90

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Book No.

Project No. BRAID EQUIP Experiment No. IDEA Date 4/18/88
 Subject NOVEL BRAIDING EQUIPMENT FOR SUTURE MANUFACTURE
 Purpose DOCUMENT CONCEPTS RELATING TO SIMON DEYOUNG M/C

2175

IDEA: SIGNIFICANT IMPROVEMENTS IN SUTURE BRAID PROCESSING MAY BE ACHIEVED BY UTILIZING A NOVEL BRAID MECHANISM REFERRED TO AS SIMON DE YOUNG CO. THE MECHANISM IS BASED ON THE FOLLOWING FEATURES: (1) CARRIERS RESIDE ON TWO HORIZONTAL PLANES VS. ONE FOR CONVENTIONAL BRAIDERS, (2) CARRIERS MOVE IN CIRCULAR PATH VS. SERPENTINE PATH FOR CONVENTIONAL BRAIDERS, AND (3) INTERLACING OCCURS BY DIVERSION OF STRAND PATH OF LOWER PLANE OF CARRIERS BY A MOVING YARN GUIDE.

IMPROVEMENTS IN SUTURE BRAID PROCESSING MAY INCLUDE:

- 1) LONGER PROCESS RUNS - CARRIER PACKAGE DIAMETER IS INCREASED SINCE CARRIERS RESIDE ON 2 PLANES WHICH ALLOWS MORE YARN / BOBBIN. LONGER BOBBINS → MORE ECONOMICAL SINCE LESS SET-UP TIME
- 2) HIGHER BRAIDER SPEEDS - DUE TO CIRCULAR CARRIER PATH VS SERPENTINE. MORE ECONOMICAL + SHORTEN EXPOSURE TIMES FOR ABSORBABLE MATERIALS.
- 3) IMPROVEMENT IN BRAID UNIFORMITY - MORE CONSTANT YARN TENSION DURING BRAIDING SINCE DISTANCE FROM BOBBIN TO BRAIDING PT REMAINS CONSTANT THROUGHOUT REVOLUTION (VS SERPENTINE PATH + FLUCTUATING TENSION) TRANSLATES TO IMPROVED SMOOTHNESS + HAND

DePuy Mitek, Inc. v. Arthrex, Inc.

C.A. No. 04-12457 PBS

DMI002611

Investigator

Witness

Crawford Britt

Date

Date

4/18/88

3-15-90

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2175
 Project No. IFI Experiment No. 5/12/88
 Subject DEFINE CONSTRUCTIONS AND YARN INFO FOR IFI BRAIDS
 Purpose IFI CONSTRUCTIONS + YARN INFO

BACKGROUND: A CONCEPT WAS FORWARDED BY DR. E. BRODYER + SUTURE DEVELOPMENT TO PRODUCE A MONOFILAMENT LIKE SUTURE BY BRAIDING 2 DIFFERENT POLYMER FIBER TYPES WITH A DIFFERENTIAL IN T_m AND SUBSEQUENTLY MELTING THE LOWER T_m FIBER TO FORM A MATRIX AROUND THE HIGHER T_m FIBER REINFORCEMENT. WORK WAS TO BE PERFORMED IN CONJUNCTION WITH THE ISRAELI FIBER INSTITUTE (IFI)

PURPOSE: DEFINE BRAID CONSTRUCTIONS AND DOCUMENT YARN LOT INFO FOR IFI BRAIDS
 TWO TYPES OF BRAID COMPOSITES ARE SUGGESTED BY DR. BRODYER: 1) ROOT BRAIDS - CONE + SHEATH ARE DIFFERENT FIBERS AND 2) RMP OR "REINFORCED MONOFILAMENT" WHERE THE 2 FIBERS ARE BLENDED IN THE CONE + SHEATH.
 IFI BRAID CONSTRUCTIONS TO BE PROCESSED INCLUDE:

IFI BRAID CONSTRUCTIONS							
IFI- FIBER	FIBER	SHEATH	SHEATH	SHEATH	CORE	CORE	
1	2	X	FIB 1	FIB 2	FIB 1	FIB 2	
TYPE	TYPE	CORE CARRIERS	DENIER	DENIER	DENIER	DENIER	
1	VIC	PDS	8X3	28	*	*	60
2	VIC	PDS	4X5	52	*	*	48
3	PET	PP	4X3	40	*	*	86
4	VIC	PDS	8X3	56	*	*	60
5	VIC	PDS	12X5	28	*	*	60
6	PET	PP	8X3	40	*	*	100
7	PET	PP	8X3	30	20	70	*
8	PET	PP	12X3	20	20	55	*
9	VIC	PDS	8X1	52	24	*	60
10	PET	PP	8X3	20	20	55	60
11	VIC	PDS	12X1	28	24	*	60
12	VIC	PDS	8X1	28	48	52	*
13	PET	PP	8X3	20	20	*	100
14	VIC	PDS	12X3	14	24	14	48
15	PET	PP	8X3	20	*	*	86

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 DMI002612

Investigator

Witness

Date

Date

5/12/88

3-15-90

No.

No.

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Project No. 16211-STG Experiment No.

Date

4/15/88

Subject: DIE-DRAWING TRIALS OF STS PTFE BRAIDS / INCOMING YARN VARIABILITY

Purpose:

PROCEDURE: DIE-DRAWING OF PTFE BRAIDS PERFORMED PER AL HUNTER'S "PROCESS TRANSFER MEMO OF STS SUTURES" OF 10/29/87, SUCH AS (1) BRAID WAS DRAWN THRU STEEL WIRE DIES, (2) BRAID WAS SIMULTANEOUSLY BEING HOT-STRETCHED USING GODET SET-UP AND A FORCED CONVECTION TUNNEL OVEN AT 315°F, AND (3) MULTIPLE PASSES WITH DECREASING DIE SIZE.

RESULTS

- DIE-DRAWING SIGNIFICANTLY REDUCES THE BRAID PROFILE OF THE PTFE BRAIDS IN ALL CASES IN THE "UNPERTURBED" OR RELAXED CONDITION. HOWEVER, A LOW AMOUNT OF TORSION OR EVEN BENDING OF THE SUTURE TYPICAL OF THE MANIPULATION REQUIRED FOR KNOT TIE-DOWN RESULTS IN A DRASTIC OPENING UP OF THE BRAID STRUCTURE. THUS, THE BRAID STRUCTURE IS APPARENT IN USE ALTHOUGH IT APPEARS 'MONOFILAMENT-LIKE' IN THE RELAXED CONDITION.
- PRODUCT UNIFORMITY (DIAMETER) IS CRITICAL IN THE DIE-DRAWING OPERATION WITH THE RISKS OF FREQUENT LINE BREAKAGE ^{OVERSIZED} (LARGE REGIONS) AND ROUGH (UNDERSIZED REGIONS) FOR VARIABLE MATERIAL. THIS MOST LIKELY RESULTS FROM THE APPARENT LARGE VARIATIONS IN YARN DENIER (AND DIAMETER) OF THE DUPONT TEFLON YARN. TYPICAL DEVIATIONS WERE:

DUPONT LABELED

DEN

66

64

88

ETHILON

MEAS. DEN

88

83

102

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Witness

Date

4/15/88

Date

2-15-90

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Book No.

Project No. BRAID EQUIP Experiment No. IDEA Date 4/19/88
 Subject NOVEL BRAIDING EQUIPMENT FOR SUTURE MANUFACTURE
 Purpose DOCUMENT CONCEPTS RELATING TO SIMON DE YOUNG M/C

2175

IDEA: SIGNIFICANT IMPROVEMENTS IN SUTURE BRAID PROCESSING MAY BE ACHIEVED BY UTILIZING A NOVEL BRAID MECHANISM DERIVED FROM DE YOUNG CO. THE MECHANISM IS BASED ON THE FOLLOWING FEATURES: (1) CARRIERS RESIDE ON TWO HORIZONTAL PLANES VS. ONE FOR CONVENTIONAL BRAIDERS, (2) CARRIERS MOVE IN CIRCULAR PATH VS. SERPENTINE PATH FOR CONVENTIONAL BRAIDERS, AND (3) INTERLACING OCCURS BY DIVERSION OF STRAND PATH OF LOWER PLANE OF CARRIERS BY A MOVING YARN GUIDE.

IMPROVEMENTS IN SUTURE BRAID PROCESSING MAY INCLUDE:

- 1) LONGER PROCESS RUNS - CARRIER PACKAGE DIAMETER IS INCREASED SINCE CARRIERS RESIDE ON 2 PLANES WHICH ACCOMMODATES MORE YARN/BOBBIN. LONGER BOBBINS → MORE ECONOMICAL SINCE LESS SET-UP TIME.
- 2) HIGHER BRAIDER SPEEDS - DUE TO CIRCULAR CARRIER PATH VS. SERPENTINE. MORE ECONOMICAL + SHORTEN EXPOSURE TIMES FOR ABSORBABLE MATERIALS.
- 3) IMPROVEMENT IN BRAID UNIFORMITY - MORE CONSTANT YARN TENSION DURING BRAIDING SINCE DISTANCE FROM BOBBIN TO BRAIDING PT REMAINS CONSTANT THROUGHOUT REVOLUTION (VS. SERPENTINE PATH + FLUCTUATING TENSION). TRANSLATES TO IMPROVED SMOOTHNESS + HAND.

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C.A. No. 04-12457 PBS
DMI002614

Investigator

Witness

Crawford Britt

Date

Date

4/19/88

3-15-90

Project No. IFI Experiment No. _____ Date 5/12/88
 Subject DEFINE CONSTRUCTIONS AND YARN INFO FOR IFI BRAIDS
 Purpose IFI CONSTRUCTIONS + YARN INFO

BACKGROUND: A CONCEPT WAS FORWARDED BY DR. E. BRODER + SUTURE DEVELOPMENT TO PRODUCE A MONOFILAMENT LIKE SUTURE BY BRAIDING 2 DIFFERENT POLYMER FIBER TYPES WITH A DIFFERENTIAL IN T_M AND SUBSEQUENTLY MEETING THE LOWER T_M FIBER TO FORM A MATRIX AROUND THE HIGHER T_M FIBER REINFORCEMENT. WORK WAS TO BE PERFORMED IN CONJUNCTION WITH THE ISRAELI FIBER INSTITUTE (IFI)

PURPOSE: DEFINE BRAID CONSTRUCTIONS AND DOCUMENT YARN LOT INFO FOR IFI BRAIDS. TWO TYPES OF BRAID COMPOSITES ARE SUGGESTED BY DR. BRODER: 1) ROOT BRAIDS - CORE + SHEATH ARE DIFFERENT FIBERS AND 2) RMP OR "REINFORCED MONOFILAMENT" WHERE THE 2 FIBERS ARE EARLIER BLENDED IN THE CORE + SHEATH. IFI BRAID CONSTRUCTIONS TO BE PROCESSED INCLUDE:

IFI BRAID CONSTRUCTIONS							
IFI-	FIBER 1	FIBER 2	SHEATH X	SHEATH FIB 1	SHEATH FIB 2	CORE FIB 1	CORE FIB 2
	TYPE	TYPE	CORE CARRIERS	DENIER	DENIER	DENIER	DENIER
1	VIC	PDS	8X3	28	*	*	60
2	VIC	PDS	4X5	52	*	*	48
3	PET	PP	4X3	40	*	*	86
4	VIC	PDS	8X3	56	*	*	60
5	VIC	PDS	12X5	28	*	*	60
6	PET	PP	8X3	40	*	*	100
7	PET	PP	8X3	30	20	70	*
8	PET	PP	12X3	20	20	55	*
9	VIC	PDS	8X1	52	24	*	60
10	PET	PP	8X3	20	20	55	60
11	VIC	PDS	12X1	28	24	*	60
12	VIC	PDS	8X1	28	48	52	*
13	PET	PP	8X3	20	20	*	100
14	VIC	PDS	12X3	14	24	14	48
15	PET	PP	8X3	20	*	*	86

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 Date 2-15-90

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Experiment No.

Date 5/12/88

Subject

IFF BRAID CONSTRUCT + YARN LOT ID

Purpose

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IFF - CONT FROM PG. 6

VICRYL/PDS AND PET/PP COMPOSITES ARE TO BE
PROCESSED FROM THE FOLLOWING YN LOTS:

IFI YARN LOT INFORMATION									
IFI FIBER #	FIBER 1	FIBER 2	SHEATH FIB 1 DENIER	SHEATH FIB 1 LOT #	SHEATH FIB 2 DENIER	SHEATH FIB 2 LOT #	CORE FIB 1 DENIER	CORE FIB 1 LOT #	CORE FIB 2 DENIER
1	VIC	PDS	28	XC3374	*	*	*	*	60
2	VIC	PDS	52	XC3349	*	*	*	*	48
3	PET	PP	40	40/27-R14-56	*	*	*	*	86
4	VIC	PDS	56	XC-3371	*	*	*	*	60
5	VIC	PDS	28	XC-3181	*	*	*	*	60
6	PET	PP	40	40/27-R14-56	*	*	*	*	100
7	PET	PP	30	30-20-R14-56	20	21.4-PP-005	70	70-34-R14-55	*
8	PET	PP	20	20-10-RXX-56	20	20.7-PP-004	55	55-27-R02-52	*
9	VIC	PDS	52	52-26-C3388	24	24-2-PY-003	*	*	60
10	PET	PP	20	20-10-R02-56	20	PP-004	55	55-27-R02-52	60
11	VIC	PDS	28	XC3374	24	PY-37-2-0	*	*	60
12	VIC	PDS	28		48		52		*
13	PET	PP	20	20-10-R02-56	20	*	*	PP-004	100
14	VIC	PDS	14	*	24	*	14	*	48
15	PET	PP	20	20-10-R02-56	*	*	*	*	86

BRAID PROCESS CONDITIONS, HOT-STRETCH PARAMETERS AND
PROPERTIES OF THE IFF BRAIDS WILL BE
SUMMARIZED AT A FUTURE DATE

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DMI002616

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Date

Date

5/12/88

2-15-90

Project No. COMPOSITE BRAIDS Experiment No. (CBE) Date 6/6/88
 Subject COMPOSITE BRAD EVAL - BRAD CONSTRUCTIONS, YARN LOT, IN PROCESS
 Purpose _____

BACKGROUND: A PRELIMINARY EVALUATION OF COMPOSITE BRAIDS, i.e. BRAIDED SUTURES CONSTRUCTED OF TWO OR MORE FIBER TYPES DESIGNED TO REALIZE THE BENEFICIAL PROPERTIES OF EACH POLYMER. COMPOSITES TO BE EVALUATED INCLUDE PET/PTEE, PET/PP AND (ABSORBABLE) PDS / VICRYL. FOUR PROCESS METHODOLOGIES WILL BE EMPLOYED TO COMBINE THE DIFFERENT FIBER TYPES INTO COMPOSITE BRAIDS:

1) CARRIER BLENDING: BLENDING IS ACCOMPLISHED DURING BRAIDING BY DIVIDING THE CARRIERS INTO TWO SETS WITH YARN A RESIDING ON ONE SET AND YARN B ON THE OTHER.

2) YARN BLENDING: BLENDING IS ACCOMPLISHED PRIOR TO BRAIDING BY PLYING YARNS A + B TOGETHER FIRST TO FORM A COMPOSITE YARN.

3) FIBER COMMINGLING - BLENDING IS ACCOMPLISHED ON FIBER LEVEL BY THE "COMMINGLING PROCESS" (CONCORDIA, RI) IN WHICH FIBERS A + B ARE INTIMATELY INTERMINGLED MOST LIKELY BY AIR-JET

4) BICOMPONENT FIBERS: BLENDING IS ACCOMPLISHED ON THE FIBER LEVEL BY EXTRUSION OF TWO POLYMERS (CO-CENTRIC) PER FILAMENT.

THE LEVEL OF BLEND HOMOGENEITY INCREASES FROM 1 → 4.

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Date

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DMI002617

CBE

Experiment No.

Date _____

6/6/88

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Subject.

CONTINUED

Purpose.

THE INITIAL COMPOSITE BRAND EVALUATION WILL FOCUS ON 15 CONSTRUCTIONS OF PET/PPE, VICAR/PPS, + PET/PP BLENDS:

COMPOSITE BRAID EVALUATION
BRAID CONSTRUCTIONS

MGS	COMP	BRAID	SIZE	SHXCR	FIBER	DEN	FIBER	FIBER	DEN	FIBER	FIBER	DEN	FIBER	FIBER	DEN	FIBER	FIBER	DEN	FIBER
ID#	TYPE	TYPE		CARR.	A	A	A	B	B	B	C	C	C	C	C	C	C	C	C
							VOLUM		VOLUM			VOLUM		VOLUM		VOLUM	SH	CARR	SH
							FRACT		FRACT			FRACT		FRACT		FRACT	FIB	FIB	FIB
CBE-01	CB	CS	X-0	8x3	PET	70		PTFE	75	*	*			1-70	2-8VE	1-3	1-3	1-3	1-3
CBE-02	YB	CS	X-0	8x3	PET	70		PTFE	75	*	*			1-8	1-8	1-3	1-3	1-3	1-3
CBE-03	CF	CS	X-0	8x3	PET	70		PTFE	75	*	*			1-8	1-8	1-3	1-3	1-3	1-3
CBE-04	CT	CS	X-0	8x3	PET	70		PTFE	75	*	*			1-8	*	1-3	*	*	*
CBE-05	CT	CS	X-0	8x3	PET	70		PTFE	75	*	*			*	1-8	*	*	1-3	1-3
CBE-06	CB	CS	2-0	12x1	VICRYL	28	34	PDS	48	66	*	*	*	1-11V0	2-12VE1			1	1
CBE-07	YB	CS	2-0	12x1	VICRYL	28	34	PDS	48	66	*	*	*	1-12	1-12	1		1	1
CBE-08	CF	CS	2-0	12x1	VICRYL	28	34	PDS	48	66	*	*	*	1-12	1-12	1		1	1
CBE-08A	CF	CS	X-0	12x1	VICRYL	28		PDS	48		*	*	*	1-12	*	1		*	*
CBE-09	CT	CS	2-0	12x1	VICRYL	28	100	PDS	48	0	*	*	*	*	1-12	*		1	1
CBE-10	CT	CS	2-0	12x1	VICRYL	28	0	PDS	48	100	*	*	*	1-12	1-12	1		1	1
CBE-11	CF	CS	X-0	12x1	PET	70		PP	50		*	*	*	1-12	*	1		*	*
CBE-12	BF	CS	X-0	12x1	PET/PP	60		*	*		*	*	*	1-12	*	1		*	*
CBE-13	CT	CS	X-0	12x1	PET	70		PP	50		*	*	*	*	1-12	*	1		*
CBE-14	CT	CS	X-0	12x1	PET	70		PP	50		*	*	*	*	1-12	*	1		*
CBE-15	CB	CS	1	12x1	PET	70	51	PTFE	110	49	*	*	*						

MS 6/4/88

Key:

CB : CARRIER BLEND

YB = YARN BLEND

CF - COMMINGLED FIBER

BF : Bicomponent Fiber

CT = CONTROL

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Date _____

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 * No. 175 Subject CONT
 Purpose _____

YARN LOT INFORMATION FOR CBE 1-15 :

COMPOSITE BRAID EVALUATION
YARN A DESCRIPTION

MGS ID#	FIBER A	FIB A DENIER	FIB A FILAM COUNT	FIB A LOT #	FIB A COLOR	FIB A TWIST LEVEL (TP1)	FIB A TWIST (S/Z)	FIB A ENTANG LEVEL
CBE-01	PET	70	48 SUT DEV	SPZ-305	GREN	0.0 *	0	
CBE-02	PET	70	48 SUT DEV	SPZ-305	GREN	0.0 *	*	
CBE-03	PET	70	48 SUT DEV	SPZ-305	GREN	0.0 *	*	
CBE-04	PET	70	48 SUT DEV	SPX-305	GREN	0.0 *	*	
CBE-05	PET	70	48 SUT DEV	SPZ-305	GREN	0.0 *	0	
CBE-06	VICRYL 28		14 CORNELIA	ZC3606	NATR	0.0 *	0	
CBE-07	VICRYL 28		14 CORNELIA	ZC3606	NATR	0.0 *	0	
CBE-08	VICRYL 28		14 CORNELIA	ZC3606	NATR	0.0 *	0	
CBE-08A	VICRYL 28		14 CORNELIA	ZC3606	NATR	0.0 *	0	
CBE-09	VICRYL 28		14 CORNELIA	ZC3606	NATR	0.0 *	0	
CBE-10	VICRYL 28		14 CORNELIA	ZC3606	NATR	0.0 *	0	
CBE-11	PET	70	48 SUT DEV	SPZ-305	GREN	0.0 *	0	
CBE-12	PET/PP	60	0 BASF		WHIT	0.0 *	0	
CBE-13	PET	70	48 SUT DEV	SPZ-305	GREN	0.0 *	0	
CBE-14	PET	70	48 SUT DEV	SPZ-305	GREN	0.0 *	0	
CBE-15	PET	70	48 SUT DEV	SPZ-305	GREN	0.0 *	0	

COMPOSITE BRAID EVALUATION
YARN B DESCRIPTION

MGS ID#	FIBER B	FIB B DENIER	FIB B FILAM COUNT	FIB B LOT #	FIB B COLOR	FIB B TWIST LEVEL (TP1)	FIB B TWIST (S/Z)	FIB B ENTANG LEVEL
CBE-01	PTFE	75	12 DUPONT	1T153	WHIT	0.0 *	LOW	
CBE-02	PTFE	75	12 DUPONT	1T153	WHIT	0.0 *	*	
CBE-03	PTFE	75	12 DUPONT	1T153	WHIT	0.0 *	LOW	
CBE-04	PTFE	75	12 DUPONT	1T153	WHIT	0.0 *	LOW	
CBE-05	PTFE	75	12 DUPONT	1T153	WHIT	0.0 *	LOW	
CBE-06	PDS	48	4 SUT DEV	PY001	PURP	0.0 *	0	
CBE-07	PDS	48	4 SUT DEV	PY001	PURP	0.0 *	0	
CBE-08	PDS	48	8 SUT DEV	PY035	PURP	0.0 *	0	
CBE-08A	PDS	48	4 SUT DEV	PY001	PURP	0.0 *	0	
CBE-09	PDS	48	4 SUT DEV	PY001	PURP	0.0 *	0	
CBE-10	PDS	48	4 SUT DEV	PY001	PURP	0.0 *	0	
CBE-11	PP	50	16 SUT DEV	PP005	WHIT	0.0 *	0	
CBE-12	*	*	0 *	*	*	0.0 *	0	
CBE-13	PP	50	16 SUT DEV	PP005	WHIT	0.0 *	0	
CBE-14	PP	50	16 SUT DEV	PP005	WHIT	0.0 *	0	
CBE-15	PTFE	110	15 DUPONT	1T138	WHIT	0.0 *		

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Date 6/6/88

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Project No. CBE Experiment No. _____ Date _____
 Subject CONTINUED
 Purpose _____

THE YARN BLEND COMPOSITES REQUIRE A PLYING/TWISTING OPERATION BEFORE BRAIDING. PLYING WAS PERFORMED ON THE RATTI 2-FOR-1 TWISTER UTILIZING THE CONDITIONS LISTED IN THE TABLE. PROPER BALANCING OF YARN TENSION WERE REQUIRED TO PREVENT A BARBER POLE APPEARANCE:



PROPER BALANCE OF
TENSION



BARBER-POLE APPEARANCE
DUE TO MISMATCH IN
YARN ELASTIC MODULUS
AND TENSION LEVELS

COMPOSITE BRAID EVALUATION
PLIED YARN PROCESS CONDITIONS

NGS ID#	FIBER A	DENIER A	FIBER B	DENIER B	PLY CAN TWIST YARN LEVEL (TPM)	CREEL YARN	CAN YARN # BRASS DISC WTS	CREEL YARN # GLASS BEADS
CBE-01	PET	70	PTFE	75	0.0 *	*	0	0
CBE-02	PET	70	PTFE	75	3.0 B	A	0	1
CBE-03	PET	70	PTFE	75	0.0 *	*	0	0
CBE-04	PET	70	PTFE	75	0.0 *	*	0	0
CBE-05	PET	70	PTFE	75	0.0 *	*	0	0
CBE-06	VICRYL	28	PDS	48	0.0 *	*	0	0
CBE-07	VICRYL	28	PDS	48	3.0 B	A	0	1
CBE-08	VICRYL	28	PDS	48	0.0		0	0
CBE-08A	VICRYL	28	PDS	48	0.0		0	0
CBE-09	VICRYL	28	PDS	48	0.0 *	*	0	0
CBE-10	VICRYL	28	PDS	48	0.0 *	*	0	0
CBE-11	PET	70	PP	50	0.0		0	0
CBE-12	PET/PP	60	*	*	0.0		0	0
CBE-13	PET	70	PP	50	0.0		0	0
CBE-14	PET	70	PP	50	0.0		0	0
CBE-15	PET	70	PTFE	110	0.0 *	*	0	0

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Book No.

2175

Project No. MICROFIBER /MMF Experiment No. _____ Date 8/18/88
Subject MONOFILAMENT / MULTIFILAMENT HYBRID WITH MICROFIBER CORE
Purpose IDEA

IDEA: A IMPROVED SUTURE IS ENVISIONED WHICH COMBINES THE ATTRIBUTES OF MONOFILAMENTS (EASE OF TISSUE PASSAGE, NO INFECTION HARBORING INTERSTICES) AND THE ATTRIBUTES OF MULTIFILAMENT BRAIDS (PLIABILITY, KNOT STR., KNOT STABILITY, DAMAGE TOLERANCE). THE HYBRID DESIGN CONSISTS OF POTENTIALLY FOUR COMPONENTS: 1) MONOFILAMENT-LIKE SHEATH, 2) CORE MULTIFILAMENT BUNDLE, 3) SHEATH-CORE INTERFACE, AND 4) MULTIFILAMENT LINE LUBRICANT (OPTIONAL). MONOFIL. SHEATH IS PREFERABLY FORMED BY EXTRUSION OR CABLE-WRAPPING / POLISHING. SHEATH POLYMER CAN BE ADHESIONABLE OR NONADHESIONABLE, AND SHOULD BE TOUGH, LOW MODULUS, & POSSESS THE PROPER FRICTIONAL PROPERTIES.

MULTIFILAMENT LINE CONSIST OF A BUNDLE OF MANY FINE FILAMENTS (1000 AND OVER) WHICH MAY BE TWISTED OR BRAIDED. TWISTED STRUCTURES SHOULD BEHAVE WITH ENHANCED PLIABILITY, WHEREAS BRAIDED STRUCTURES SHOULD MAINTAIN ROUNDRNESS BETTER.

TWO APPROACHES ARE POSSIBLE REGARDING THE SHEATH-CORE INTERFACE. ONE IS TO MAXIMIZE ADHESION TO PREVENT TEARING / STRIPPING. IT IS BELIEVED THAT THIS WILL DETRACT FROM PLIABILITY BY INHIBITING YARN/FIBER MOBILITY. THE OTHER APPROACH IS TO MINIMIZE SHEATH-CORE ADHESION, POSSIBLY BY THE INCORPORATION OF AN OIL LIKE LUBRICANT (SILICONE OIL FOR EXAMPLE) OR SOLID LUBRICANT LIKE PTFE FIBERS IN THE CORE BUNDLE. THIS SAME LUBRICATION APPROACH MAY BE OF VALUE WITHIN THE CORE BUNDLE TO MINIMIZE FIBER-FIBER INTERACTIONS.

THE RESULTING SUTURE SHOULD HAVE E.C. TISSUE PASSAGE, PLIABILITY, KNOT PROPS, RESISTANCE TO CATASTROPHIC DAMAGE AND MINIMAL TENDENCY FOR INFECTION HARBORING.

Investigator

Witness

Date

Date 3-15-90

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Book No.

2175

Project No. STS Experiment No. _____ Date 9/27/88
 Subject TRIBOHESION PROCESSED STS BRAID SAMPLES
 Purpose SEM + PHYS. PROP. CHARACTERIZATION

BACKGROUND: 23 SAMPLES OF TRIBOHESION (LONDON, UK) PROCESSED BRAID SAMPLES WERE SUPPLIED BY MR E. NAGY IN OUR MEETING AT ETHILON ON 7/26/88. THE STRANDS WERE COMPOSED OF 2-0 STS PTFE BRAID WHICH WAS CABLE WRAPPED AND POLISHED. STRAND LENGTH WAS 1-2 M. LIMITED INFORMATION WAS RELEASED BY TRIBOHESION ON THE PROCESSING OF THE SAMPLES, BUT IT IS KNOWN THAT THE PROCESS VARIABLES INCLUDE LINE SPEED, TAPE TENSION, TAPE WIDTH + THICKNESS, AND DEGREE OF POLISHING.

RESULTS: PHYSICAL PROPERTY CHARACTERIZATION VS. ORIGINAL STS BRAID AND GORE-TEX:

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PHYSICAL PROPERTY CHARACTERIZATION

PROPERTY	UNITS	ORIGINAL 2-0 STS BRAID	TRIBOHESION PROCESSED 2-0 STS BRAID #13	GORE-TEX SIZE 4-0 MONOFILAM.
DIAMETER USP OPTICAL	(MILS) (MILS)	12.1 N/A	20.2 26.5	13.6 N/A
STR. TENSILE	(LBS)	4.1	7.8	5.0
INTRIN. TENSILE (USP DIAM)	(PSI)	35,600	24,300	34,400
ULT. ELONGATION	(%)	20.0	55.1	25.5
KNOT STRENGTH	(LBS)	3.9	7.1	4.1
INTRIN. KNOT	(PSI)	33,900	22,100	28,200
KNOT/STRAIGHT STR	(%)	95	91	82
KNOT SECURITY	(# OF THROWS)	6	5-6	6-7

N/A : not available

* : composite of several lots and sizes

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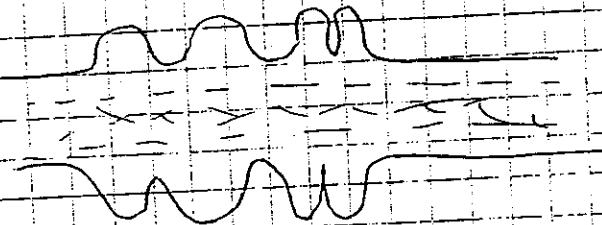
1175

Subject TRIBOTHEION

Purpose CONTINUED

SEM OBSERVATIONS:

- 1) SAMPLES WITH POOR SUBJECTIVE SMOOTHNESS POSSESSED AN OVERSIZED SHEATH WHICH DISTORTED EASILY. DISTORTION WAS EITHER A WINKLING DUE TO TORSION OR AN BELLOWS TYPE FOLDING DUE TO SHEATH SLIDING.

INTERNAL
BRAID

BELLOWS TYPE SHEATH FOLDING

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- 2) SAMPLES WITH GOOD SUBJECTIVE SMOOTHNESS APPEARED MONOPIL. LIKE AT 55X.
- 3) TAPE SEAMS WERE USABLE IN NON-POLISHED SAMPLES AT 55X.
- 4) SIGNIFICANT SHEATH DISTORTION OBSERVED AROUND KNOT, BUT NO SHEATH TEARING.
- 5) THE MICROSTRUCTURE OF THE SHEATH FILM IS EXPANDED LIKE THE GORE PRODUCT, BUT THE TRIVEX PRODUCT IS TO A LESSER DEGREE (550X)
- 6) SHEATH DISTORTION WAS EXCESSIVE IN REGIONS OF HIGH PICK DENSITY.

DISCUSSION

- PICK PROPS ARE LOW ESPECIALLY SINCE SHEATH INCL. DIAM.
- PET OR PET/PTEE GORE BRAID SHOULD BE EXPLORED
- OVERSIZED SHEATHS OUTLAST AND BECOME 'ROUGH'

Investigator

Witness

Date

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Project No. MMH Experiment No. _____ Date 10/19/88
 Subject MONOFILAMENT - MULTIFILAMENT HYBRID
 Purpose IDEA

2175

IDEA - FOLLOW UP FROM 2175-12.

THE ADDITION OF A SILICONE TYPE OIL TO THE TWISTED OR BRAIDED CORE BUNDLE CAN DRAMATICALLY IMPROVE PLIABILITY. HOWEVER, IT COULD ALSO INHIBIT WICKING OF BIOLOGICAL FLUID INTO THE FILAMENT CORE WHICH MIGHT OTHERWISE LEAD TO INFECTION. THIS HAS BEEN A PROBLEM WITH PREVIOUS APPROACHES OF THIS NATURE. THE LUBRICANT SHOULD BE HYDROPHOBIC (LOW SURFACE TENSION) AND COULD BE ABSORBABLE OR NONABSORBABLE. ALSO, FINE DPF FILAMENTS WOULD ALSO INHIBIT WICKING BY RESULTING IN A SMALLER DIAM. SIZE.

IF THE MONOFIL. SHEATH IS EXTRUDED, IT MAY BE BENEFICIAL TO FORM IT WITH AN ANNULAR DIE TO MINIMIZE THE PENETRATION OF THE MELTEN SHEATH POLYMER INTO THE CORE BUNDLE. OTHER PRECAUTIONS TO MINIMIZE SHEATH-CORE ADHESION INCLUDE RAPID SHEATH QUENCHING + DRAWING/ORIENTATION.

IN THE CASE OF ABSORBABLE HYBRIDS, LOW MW ANALOGS OF PDD, CAPROLACTONE, PGA, PLA AS DESCRIBED BY AL HUNTER MAY BE USEFUL AS THE LUBRICANTS.

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Investigator
 Witness

Mark Shacht
Crawford Britt

Date 10/19/88Date 3-15-90

Age _____
 Ink No. _____
 175
 Project No. CBE Experiment No. _____ Date 11/11/88
 Subject COMPOSITE BRAID EVALUATION
 Purpose PROCESS CONDITIONS AND PROPS

BACKGROUND: CONTINUATION OF 2175-8, 14 COMPOSITE
 BRAIDS WERE PROCESSED AND CHARACTERIZED (CONSTRUCTIONS
 AND YARN LOT INFO ON PGS 8-11). BRAID
 PROCESS CONDITIONS WERE AS FOLLOWS:

COMPOSITE BRAID EVALUATION
 BRAID PROCESS CONDITIONS

MGS ID#	BRAIDER NO.	GEAR NO.	RPM	SHEATH SPRING DIAM. (MILS)	SHEATH SPRING LENGTH (IN)	CORE TENSION TXTRL SET PT	CORE GLASS TXTRL ROD PT	CORE TENSION MEAS. (GMS)
CBE-01	6	32	183	0.009	5.0	TXTRL	1.0 Y	18
CBE-02	6	32	183	0.009	5.0	TXTRL	1.5 Y	20
CBE-03	*	*	*	0.000	0.0	*	0.0 *	0
CBE-04	6	32	183	0.009	5.0	TXTRL	1.0 Y	21
CBE-05	3	36	170	0.000	0.0	TXTRL	1.0 Y	22
CBE-06	12	32	182	0.009	5.0	TXTRL	1.0 Y	20
CBE-07	12	32	182	0.009	5.0	TXTRL	1.0 Y	17
CBE-08	*	*	*	0.000	0.0		0.0	0
CBE-08A				0.000	0.0		0.0	0
CBE-09	12	32	182	0.009	5.0	TXTRL	1.0 Y	17
CBE-10	12	32	182	0.009	5.0	TXTRL	1.0 Y	19
CBE-11				0.000	0.0		0.0	0
CBE-12				0.000	0.0		0.0	0
CBE-13	10	32	183	0.009	5.0	TXTRL	1.0 Y	18
CBE-14	12	36	182	0.009	5.0	TXTRL	1.0 Y	17

KEY:

TXTRL: TEXTROL
 TENSION
 DEVICE

THE PET/PTEE SAMPLES (CBE-01 TO 05) HAD A RANGE OF
 PROCESSING PROBLEMS ~~AS~~ SUCH AS CORE-POPPING AND LOOSENESS.
 CBE-03 WAS ABANDONED SINCE THE PTEE YARN WAS
 INTERCALATED MAKING COMMINGLING IMPOSSIBLE. CBE-01
 HAD SPRINGS ONLY ON PET CARRIERS, NO SPRINGS ON
 PTEE CARRIERS. CBE-08 (VULPOS) WAS ABANDONED SINCE
 COMMINGLING WAS IMPOSSIBLE. CBE-12 WAS DELAYED
 DUE TO SOURCING PROBLEMS WITH THE BLOOMINGTON FIBER

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Witness

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Crawford Britt

Date

Date

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Date 11/11/88

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Subject CONTINUED

Purpose _____

FOLLOWING BRAID PROCESSING, THE MATERIALS WERE
HOT-STRETCHED ACCORDING TO THE FOLLOWING
CONDITIONS:

HOT STRETCH CONDITIONS

MGS ID#	HOT-STRETCH %	ROLL 1 FPM	ROLL 2 FPM	ROLL 1 # OF WRAPS	ROLL 2 # OF WRAPS	ZONE 1 TEMP (C)	ZONE 2 TEMP (C)	ZONE 3 TEMP (C)	ZONE 4 TEMP (C)
CBE-01	30	9.0	11.7	8	12	125	150	190	225
CBE-02	30	9.0	11.7	8	12	125	150	190	225
CBE-03	0	0.0	0.0	0	0	0	0	0	0
CBE-04	30	9.0	11.7	8	12	125	150	190	225
CBE-05	30	9.0	11.7	8	12	125	150	190	215
CBE-06	10	9.0	9.8	8	12	125	150	190	215
CBE-07	10	9.0	9.8	8	12	125	150	190	215
CBE-08	0	0.0	0.0	0	0	0	0	0	0
CBE-08A	0	0.0	0.0	0	0	0	0	0	0
CBE-09	10	9.0	9.8	8	12	125	150	190	215
CBE-10	10	9.0	9.8	8	12	125	150	190	215

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INITIAL PHYSICAL PROPERTY CHARACTERIZATION YIELDED THE
FOLLOWING RESULTS:

PHYSICAL PROPERTY CHARACTERIZATION

MGS ID#	USP ULTIMAT DIAM (MILS)	ULTIMAT TENSILE STREN (LBS)	INTRIN TENSILE STREN (PSI)	ULTIMAT TENSILE STREN (LBS)	INTRIN TENSILE STREN (PSI)	KNOT CONVER (%)	ULTIMAT ELONGAT (%)	STRAND BENDING RIGIDITY (GHXCMZ)	KNOT STABIL (# THROWS)	PICKS PER INCH	TOTAL DENIER
CBE-01	0.0	0.00	0	0.00	0	0	0	0.00			
CBE-02	0.0	0.00	0	0.00	0	0	0	0.00			
CBE-03	0.0	0.00	0	0.00	0	0	0	0.00			
CBE-04	0.0	0.00	0	0.00	0	0	0	0.00			
CBE-05	0.0	0.00	0	0.00	0	0	0	0.00			
CBE-06	10.7	6.79	75450	4.37	48580	64	29	0.00 *		46	1058
CBE-07	13.9	10.16	66930	6.46	42808	64	28	0.00 *		45	1019
CBE-08	0.0	0.00	0	0.00	0	0	0	0.00			
CBE-08A	0.0	0.00	0	0.00	0	0	0	0.00			
CBE-09	14.1	15.70	100540	7.98	51490	51	29	0.00 *		44	1099
CBE-10	10.9	7.00	75030	4.47	47650	64	42	0.00 *		51	612

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THE PROPERTIES OF THE COMPOSITES ARE AS EXPECTED MIDWAY
BETWEEN THE CONTROLS.

Investigator

Witness

Paul Stecher
Crawford Britt

Date

Date 3-15-90

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Work No.

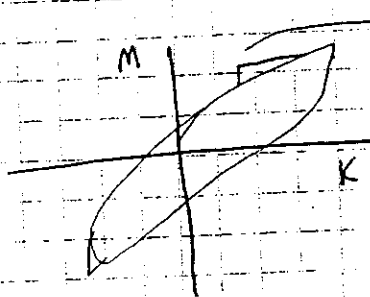
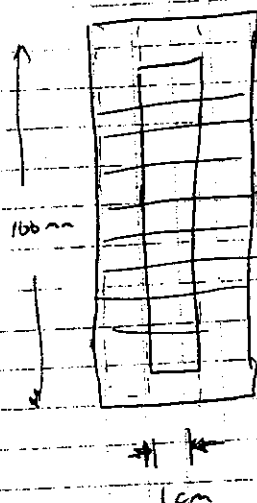
Project No. KAWABATA Experiment No. _____ Date 11/15/88
 Subject KAWABATA BENDING RIGIDITY TESTING
 Purpose INITIAL RESULTS OF BENDING TESTING

1175

BACKGROUND: THE KAWABATA BENDING RIGIDITY TESTER AT PHILA. COLLEGE OF TEXTILES + SCIENCE WAS UTILIZED TO MEASURE THE PLIABILITY OF BRAIDED SUTURES.

PROCEDURE:

AN ARRAY OF PARALLEL STRANDS OF BRAIDED SUTURES WERE MOUNTED BETWEEN TWO CARDBOARD TABS AS SHOWN BELOW. TYPICALLY 40 ENDS WERE USED ALTHOUGH THIS VARIES WITH THE SUTURE SIZE. THE KAWABATA TESTER MEASURES THE TORQUE AS A FUNCTION OF BENDING CURVATURE OF THE PARALLEL SUTURES. THE BENDING RIGIDITY



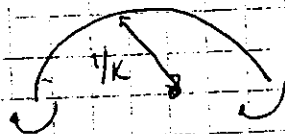
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$$K = 1/r$$

r = BENDING RADIUS

K = CURVATURE

M = BENDING MOMENT



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IS THE SLOPE OF THE BENDING MOMENT - CURVATURE PLOTS.
 THE FOLLOWING VALUES WERE OBTAINED IN OFF-BRAIDED + HOT-STRETCH. POLYESTER:

	SIZE →	6-0	4-0	2-0	0	2
BENDING RIGIDITY	OFF-BRAIDED	.004	0.026	0.029	0.036	.087
(GM-CM/STRAND)	HOT-STRETCHED	.002	0.024	0.253	0.103	0.267

AS EXPECTED, THE EI GENERALLY INCR. AS SIZE INCREASES,
 AND ALSO INCR. W/ HOT-STRETCHING.

Investigator

Witness

Date

Date

11/15/88

2-15-90

Project No. BCAD Experiment No. _____ Date 11/18/88
 Subject BRAID CAD - MODEL CONSTRUCTIONS
 Purpose DEFINE MODEL CONSTRUCTIONS

2175

BACKGROUND: THE JOINT DEVELOPMENT PROGRAM BETWEEN ETHICON + DREXEL UDU IS TO OFFER SOFTWARE TO DESIGN BRAIDED SUTURES. EXPERIMENTAL DATA IS REQUIRED ON SIMPLE, WELL-BEHAVED BRAIDED GEOMETRIES IN ORDER TO CONFIRM THE THEORETICAL PREDICTIONS. THE FOLLOWING CONSTRUCTIONS HAVE BEEN CHOSEN FOR DUPONT DACRON PET TYPE 52:

CARRIERS	CORE	PICK	GEARS	
3	0	22	26	30
4	0	26	30	34
8	0	28	32	36
8	1	28	34	36
12	2	28	32	36
16	3	26	30	34

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THE ABOVE CONSTRUCTIONS ARE TO BE MADE WITH YARN WITH PRODUCER'S TWIST. TO EVALUATE THE EFFECT OF TWIST, A SMALLER SET OF SAMPLES HAS BEEN DESIGNED:

CARRIERS	CORE	PICK GEAR	TWIST LEVELS
8	1	34	0, 1.5, 3, 6

TENSILE, DIAMETER, SURFACE PROPS, BENDING RIGIDITY CHARACTERIZATION WILL BE PERFORMED ON ALL ABOVE BRAIDS.

Investigator

Witness

Mal Fletcher
Paul L. Britt

Date

Date

11/18/88

3-15-90

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Project No. DUPONT Experiment No. _____ Date 12/7/88
 Subject DUPONT HOLLOW + MULTILOBAL FIBER EVALUATION
 Purpose EVALUATE EXPERIMENTAL MATERIALS

BACKGROUND: TWO EXPERIMENTAL DACRON PET YARNS
 WERE PROVIDED BY DUPONT FOR EVALUATION AS
 SUTURE YARNS. YARN DESCRIPTIONS ARE GIVEN
 IN TABLE 1: (1) MULTILOBAL (2) HOLLOW

TABLE 1.
Exploratory Dupont Yarn

1. Dacron 50 den 34-R14
 Textile Yarn Rotoset
 Semidull Type 929 Tube
 Reference 7184 Merge 12601
2. Nylon 30 den 10-R25
 Textile Yarn Rotoset
 Dead Bright Type 335
 Reference 40244 Merge 18681
3. Nylon 70 den -66-R25-295-M
 Merge 64402
4. Polyester Hollow Multifilament Yarn
 Round Semi-dull
 71.6 den 50 filaments
 Void size : 13.8%
 Tenacity: 5.0 gpd Modulus: 90.4 gpd Elong.: 16.0%
 Finish 0.65-1.00%

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PROCESS CONDITIONS

DUPONT HOLLOW AND MULTILOBAL FIBER BRAIDS

THE YARNS WERE
 PROCESSED INTO
 BRAIDS ACCORDING
 TO MERSILENE
 PROCESS SPECS
 FOR SIMILAR DEN
 YARN. THE BRAIDS
 WERE STRETCHED +
 HOT-STRETCHED TO
 MERSILENE SPECS
 (SEE TABLE 2)

PARAMETER	DFE-1	DFE-2
Fiber Type	Multilobal	Hollow
Denier/Filaments	50/34	72/50
Construction	16x3	12x1 MS
Pick gear	30	12
RPM	174	174
Sheath springs	none	0.009x5"
Core tension set	1.0	1.0
Hot str %	15	15
H S Temp (F)	225	225

Investigator
 Witness

[Signature]
[Signature]

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Project No. DUPONT

Experiment No.

Date 12/7/88Subject CONTINUED

Purpose

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RESULTS:

THE HOT-STRETCHED BRAIDS WERE CHARACTERIZED
 ACCORDING TO STANDARD PHYS. PROP. TESTING AND
 ARE COMPARED TO STANDARD MERSILENE HOT-STR.
 BRAIDS:

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SUTURE PHYSICAL PROPERTIES
 STANDARD AND SPECIALTY DACRON PET FIBER BRAIDS

MATERIAL DESCRIP.	DIAM. (DIAM)	TENSL. STREN. (LBS)	INTRIN. TENSL. STREN. (KSI)	ELONG. (%)	KNOT STREN. (LBS)	INTRIN. KNOT STREN. (KSI)
DPE-1 MULTI- LOBAL PET 50-34-R14 SIZE 2-0	12.8	6.4	49.4	40.5	5.2	40.5
MERSILENE SIZE 2-0 GREEN	12.7	14.2	112.1	11.0	7.1	56.1
DPE-2 HOLLOW PET 72-50 SIZE 0	14.4	10.7	65.7	28.3	7.2	44.1
MERSILENE SIZE 0 GREEN	15.0	15.2	87.7	16.0	8.9	50.4

MS

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DISCUSSION:

THESE YARN TYPES APPEAR TO OFFER NO SIGNIF. IMPROVEMENTS
 IN SUTURE PROPS. STRAIGHT + KNOT TENSILES ARE
 SUBSTANTIALLY LOWER IN BOTH CASES. KNOT CONVERSION
 IS RELATIVELY GOOD FOR MULTILOBAL (82% VS 50% FOR
 THE 2-0 CONTROL), HOWEVER IT IS NOT CLEAR WHETHER
 THIS IS DUE TO X-SHAPED SHAPE OR LOWER MODULUS YARN.

Investigator

Witness

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 Crawford Britt

Date

Date

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Project No. PDS Experiment No. 2 * 12 DPF EVALUATION Date 12/14/88
 Subject PDS BRAIDS - 2 * 12 DPF EVALUATION
 Purpose EVALUATE BIOLOGICAL & PHYSICAL PROPERTIES

PROCEDURE: PDS MULTIFILAMENT YARNS WERE BRAIDED AND EVALUATED FOR BIOLOGICAL PROPERTIES AND (IN VITRO AND INVIVO). THE YARN WAS OBTAINED FROM DR. E. BROKEN AND POSSESSED THE FOLLOWING PROPS:

Properties of PDS* Yarns

sample	denier	dpf	tenacity g/den	elong. %
RLS-248E	58.7	11.74	6.75	63
QPY-022-3-2	74.9	14.98	4.8	21
QPY-023-5-1	67.3	13.46	5.6	21
PY-045	57.8	2.06	5.25	59.95

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ALL YARN WAS BRAIDED PER VICRYL 2-0 SPECIFICATION THE FOLLOWING COMPARES THE INVIVO AND INVITRO DATA VS. PDS MONOFILAMENT AND VICRYL BRAID:

PDS BRAID IN VITRO PERFORMANCE

BRAID ID	FIBER YARN DPF ID	BRAID SIZE	BASLINE TENSILE (PSI)	IN VITRO 5 DAY TENSILE % BSR	PDS MONOFIL TENSILE (PSI)	PDS MONOFIL IN VITRO 5D %BSR	VICRYL BRAID TENSILE (PSI)	VICRYL BRAID IN VITRO 12D %BSR	INVIVO 21 DAY %BSR
CBS-001	2.1 PY-045	2-0	70930	23.6	87490	64.2	112300	54.8	3
CBS-002	15.0 QPY-022	2-0	57300	34.9	87490	64.2	112300	54.8	22
CBS-003	11.7 RLS-248E	2-0	70270	47.1	87490	64.2	112300	54.8	26
CBS-004	13.5 QPY-023	3-0	61350	48.7	95440	82.1	120150	56.2	36

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DISCUSSION:

THE 2 DPF PRODUCT HAS EXCEPTIONALLY POOR BSR - 3% AT 21 DAY VS APPROX 50% FOR VICRYL 2-0. THE 2 * 12 DPF PRODUCT WERE SIGNIFICANTLY BETTER BUT STILL INFERIOR TO VICRYL OR PDS MONOFIL. THE HAND OF THE PRODUCT WAS ALSO INFERIOR TO VICRYL FROM A STIFFNESS VIEWPOINT. THE 2-0 DPF POSSESSED A HIGH # OF BROKEN FIBERS WHICH CONTRIBUTED TO BRAID ROUGHNESS.

Investigator

Witness

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Project No. IFI Experiment No. _____ Date 12/14/88
 Subject BRAID PROCESS CONDITIONS, H.S. CONDITIONS, PAYS PROP. CHARACTER.
 Purpose CHARACTERIZATION OF COMPOSITE IFI BRAIDS

2175

CONTINUATION FROM Pg. 6:

BACKGROUND: ROOT AND RMS VILAYL/PDS + PET/PP
 BRAID CONSTRUCTIONS HAVE BEEN DEFINED PREVIOUSLY.
 BRAIDS WERE PROCESSED ACCORDING TO FOLLOWING
 CONDITIONS:

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IFI BRAID PROCESS CONDITIONS												
IFI LAB # ID #	SIZE	TYPE	FIBER 1	FIBER 2	PICK GEAR	SHEATH SPRING DIAM. x LENGTH	CORE TENS SET	CORE TENS MEAS (GMS)	BRAIDER RPM	PLY TWIST (TPI)		
1	SBZ-020	4-0	ROOT	VIC	PDS	27	NONE	TXTL 0.0	12	160 *		
2	SBZ-007	4-0	ROOT	VIC	PDS	20	NONE	BUTT NONE		180 *		
3	SBZ-009	4-0	ROOT	PET	PP	29	NONE	NONE *	*	180 *		
4	SBZ-005	3-0	ROOT	VIC	PDS	30	9x5.0	NONE *	*	160 *		
5	SBZ-006	3-0	ROOT	VIC	PDS	30	9x5.0	NONE *		180 *		
6	SBX-010	3-0	ROOT	PET	PP	30	9x5.0	BUTT 9x5.0		183 *		
7	SBZ-023	3-0	RMF	PET	PP	31	9x5.0	TXTL		160 3.0		
8	SBZ-022	3-0	RMF	PET	PP	30	9x5.0	TXTL 0	20	182 3.0		
9	SBZ-021	3-0	RMF	VIC	PDS	27	9x5.0	TXTL	12	182 3.0		
10	SBZ-025	3-0	RMF	PET	PP	31	NONE	TXTL	35	160 3.0		
11	SBZ-024	3-0	RMF	VIC	PDS	31	9x5.0	TXTL		183 3.0		
12	SBZ-028	3-0	RMF	VIC	PDS	--	--	----	---	0 ---		
13	SBZ-027	3-0	RMF	PET	PP	31	NONE	TXTL	26	160 3.0		
14	*	3-0	RMF	VIC	PDS	*	*	* *	*	0 *		
15	SBZ-013	4-0	ROOT	PET	PP	27	NONE	BUTT	80	182 3.0		

CORE COILING WAS A CONSIDERABLE PROBLEM IN NEARLY
 ALL BRAIDS DUE TO MISMATCHES IN ELASTIC MODULI.

ALL MATERIALS WOUND ON HALOAT AND BRAIDED
 ON W.E. BUTTS. TEXTURE TENSION CONTROL UNITS
 WERE USED ON CORE YARNS.

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Project No. IFI Experiment No. _____ Date 12/14/88
 Subject _____
 Purpose CONTINUED

AFTER BRAIDING AND APPROPRIATE SLOWING (ETAL FOR VIC/PDS, AQUEOUS DETERGENT FOR PP/PET), THE BRAIDS WERE HOT-STRETCHED IN A FORCED CONVECTION TUNNEL AT THE FOLLOWING CONDITIONS:

IFI BRAID HOT-STRETCH CONDITIONS

IFI LAB #	ID#	FIBER 1	FIBER 2	HOT-STRET PERCN (%)	GODET 1 FPM	GODET 1 WRPS	GODET 2 WRPS	ZONE 1 TEMP (F)	ZONE 2 TEMP (F)	ZONE 3 TEMP (F)	ZONE 4 TEMP (F)
1	SBZ-020	VIC	PDS	*	0.0	0	0.0	0	0	0	0
2	SBZ-007	VIC	PDS	22	9.0	9	11.0	125	150	175	195
3	SBZ-009	PET	PP	35	7.0	7	10.7	122	146	170	194
4	SBZ-005	VIC	PDS	11	9.0	7	10.0	122	146	170	194
5	SBZ-006	VIC	PDS	22	9.0	7	11.0	125	150	175	195
6	SBZ-010	PET	PP	34	8.0	7	10.7	175	225	250	300
7	SBZ-023	PET	PP	34	8.0	8	10.7	175	225	250	300
8	SBZ-022	PET	PP	34	8.0	7	10.7	175	225	250	295
9	SBZ-021	VIC	PDS	10	10.0	7	11.0	125	150	175	195
10	SBZ-025	PET	PP	34	8.0	7	10.7	175	225	250	295
11	SBZ-024	VIC	PDS	34	8.0	9	10.0	125	150	175	195
12	SBZ-028	VIC	PDS	--	0.0	0	0.0	0	0	0	0
13	SBZ-027	PET	PP	--	0.0	0	0.0	0	0	0	0
14	*	VIC	PDS	*	0.0	0	0.0	0	0	0	0
15	SBZ-013	PET	PP	34	8.0	7	10.7	175	225	250	300

A HIGHER THAN PREFERRED HOT-STRETCH RATIO WAS SOMETIMES REQUIRED IN ORDER TO REMOVE THE WIDE-SPREAD BONE-POPS.

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Subject

CONT.

Purpose

THE FOLLOWING ARE THE PHYSICAL PROPERTIES OF
THE IFI BRAIDS. THE BRAIDS

IFI BRAID COMPOSITES
TEST RESULTS

IFI TYPE	FIBER 1	FIBER 2	SIZE	DIAM (MILS)	TENSL STD. DEV.	TENSL (LBS)	STD. DEV.	INTRIN TENS (PSI)	KNOT TENS (LBS)	STD. DEV.	INTRIN TENS (PSI)	ELONG (%)	STD. DEV.
2	ROOT VIC	PDS	4-0	8.9	0.1	5.5	0.2	87.8	3.6	0.3	57.7	25.7	1.3
3	ROOT PET	PP	4-0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4	ROOT VIC	PDS	3-0	10.3	0.0	7.8	0.4	93.7	4.8	0.2	57.9	29.2	2.2
5	ROOT VIC	PDS	3-0	10.4	0.2	6.6	0.1	0.0	4.2	0.5	0.0	16.9	1.2
6	ROOT PET	PP	3-0	10.9	0.0	6.1	0.2	65.8	4.4	0.2	47.5	28.2	3.1
7	RMF PET	PP	3-0	11.6	0.2	6.7	0.1	0.0	4.7	0.2	0.0	31.8	1.5
8	RMF PET	PP	3-0	12.9	0.1	7.9	0.1	0.0	5.4	0.2	0.0	24.1	1.0
9	RMF VIC	PDS	3-0	11.0	0.1	8.3	0.2	0.0	4.4	0.2	0.0	34.0	1.6
10	RMF PET	PP	3-0	12.7	0.1	7.5	0.1	0.0	5.0	0.3	0.0	22.4	0.7
11	RMF VIC	PDS	3-0	10.5	0.2	7.5	0.1	0.0	5.0	0.3	0.0	21.0	0.6
12	RMF VIC	PDS	3-0	12.6	0.1	11.2	0.2	0.0	6.4	0.2	0.0	28.2	1.2
13	RMF PET	PP	3-0	7.8	0.1	4.1	0.1	0.0	2.6	0.1	0.0	12.4	1.2
14	RMF VIC	PDS	3-0	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
15	ROOT PET	PP	4-0	10.2	0.1	7.8	0.4	93.7	4.3	0.2	52.8	29.2	2.2
1	ROOT VIC	PDS	4-0	7.9	0.1	4.5	0.2	92.3	2.8	0.1	58.2	29.3	2.0

APPROXIMATELY 750 YDS OF EACH BRAID WAS
DELIVERED TO DR. E. BOYER FOR FURTHER
PROCESSING.

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Project No. CBE Experiment No. _____ Date 2/2/89
 Subject PET/PTFE COMPOSITE BRAIDS
 Purpose EXPLORATORY EVALUATION OF VARIOUS PROCESS METHODOLOGIES

BACKGROUND - PAGE 8

ADDITIONAL PET/PTFE COMPOSITES BRAIDS WERE PRODUCED UTILIZING 1) CARRIER BLEND, 2) YARN BLEND, 3) COMMINGLING TECHNOLOGIES. COMPOS OF 100% PET AND 100% PTFE WERE ALSO PRODUCED. FIBER SUPPLY/TYPE/DENIER, BRAID CONSTRUCTION, SPOOL CONDITION, H-S. CONDITIONS WERE CONSTANT FOR ALL BRAIDS.

THE FOLLOWING IS THE YARN INFORMATION/DESCRIPTION:

COMPOSITE BRAID EVALUATION YARN A DESCRIPTION

MGS ID#	FIBER A	FIB A DENIER	FIB A FILAM COUNT	FIB A SOURCE	FIB A LOT #	FIB A COLOR	FIB A TWIST (TPI)	FIB A TWIST (S/Z)	FIB A ENTANG LEVEL
CBE-15	PET	70	48	SUT DEV	SP2-305	GRN	0.0 *	0	0
CBE-16	PET	70	48	SUT DEV	SP2-305	GRN	0.0 *	0	0
CBE-16A	PET	70	34	DUPONT		WHIT	0.0 *	0	R14
CBE-17	PET	70	48	SUT DEV	SP2-305	GRN	0.0 *	0	0
CBE-18	PET	70	48	SUT DEV	SP2-305	GRN	0.0 *	0	0
CBE-19	PET	70	48	SUT DEV	SP2-305	GRN	0.0 *	0	0

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COMPOSITE BRAID EVALUATION YARN B DESCRIPTION

MGS ID#	FIBER B	FIB B DENIER	FIB B FILAM COUNT	FIB B SOURCE	FIB B LOT #	FIB B COLOR	FIB B TWIST (TPI)	FIB B TWIST (S/Z)	FIB B ENTANG LEVEL
CBE-15	PTFE	110	15	DUPONT	1T138	WHIT	0.0 *	0	0
CBE-16	PTFE	110	15	DUPONT	1T138	WHIT	0.0 *	0	0
CBE-16A	PTFE	115	15	DUPONT	1T138	WHIT	0.0 *	0	0
CBE-17	PTFE	115	15	DUPONT	1T138	WHIT	0.0 *	0	0
CBE-18	PTFE	115	15	DUPONT	1T138	WHIT	0.0 *	0	0
CBE-19	PTFE	115	15	DUPONT	1T138	WHIT	0.0 *	0	0

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Subject PET/PIVE COMPOSITES
Purpose CONTIN.

Project No. _____
Subject PET/PTVE COMPOSITES

Purpose Contin.

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Approx. 50/50 BY VOLUME BRAIDS WERE PRODUCED
IN THE FOLLOWING CONSTRUCTION + CONDITIONS:

COMPOSITE BRAID EVALUATION
BRAID CONSTRUCTIONS

MGS	COMP	BRAID	SIZE	SHXCR	FIBER	DEN	FIBER	FIBER	DEN	FIBER									
ID#	TYPE	TYPE	CARR.	A	A	A	B	B	B	B									
					VOLUM			VOLUMSH			CARR	SH	CARR	SH	CARR	CR	CARR	CR	CA
					FRACT			FRACT			FIB A	FIB B	FIB C	FIB A	FIB				
CBE-15	CB	CS	1	12x1	PET	70	51	PTFE	110	49	DIAGRM	DIAGRM	*		1				1
CBE-16	YB	CS	1	12x1	PET	70	51	PTFE	110	49	1-12	1-12	*		1				1
CBE-16A	YB	CS	1	12x1	PET	70	51	PTFE	115	49	1-12	1-12	*		1				1
CBE-17	CF	CS	1	12x1	PET	70	51	PTFE	115	49	1-12	1-12	*		1				1
CBE-18	CT	CS	1	12x1	PET	70	100	PTFE	115	*	1-12	*	*		1				*
CBE-19	CT	CS	2	12x1	PET	70	*	PTFE	115	100	*	1-12	*	*					1

COMPOSITE BRAID EVALUATION
BRAID PROCESS CONDITIONS

MGS	BRAIDER	GEAR	RPM	SHEATH	SHEATH	CORE	CORE GLASS	CORE
ID#	NO.	NO.	SPRING	SPRING	TENSION	TXTRL	ROD	TENSION
			DIAM.	LENGTH	TYPE	SET		MEAS.
			(MILS)	(IN)		PT		(GMS)
CBE-15	12	30	182	0.009	5.0	TXTRL	1.0 Y	16
CBE-16	00	31	215	0.009	5.0	TXTRL	1.0 Y	16
CBE-16A	00	36	215	0.009	5.0	TXTRL	1.0 Y	20
CBE-17	12	32	182	0.009	5.0	TXTRL	0.0 Y	14
CBE-18	12	30	182	0.009	5.0	TXTRL	1.0 Y	17
CBE-19	12	36	182	0.009	5.0	TXTRL	1.0 Y	15

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Purpose

CONTINUED

THE ABOVE BRAIDS WERE BOUNDED IN SKIN FORM
IN A BEAKER w/ AN AQUEOUS DETERGENT SYSTEM.
FOLLOWING SLOWING + ONLY, THE BRAIDS WERE
HOT-STRETCHED AS FOLLOWS:

COMPOSITE BRAID EVALUATION
HOT STRETCH CONDITIONS

MGS ID#	HOT-STRETCH %	ROLL 1 FPM	ROLL 2 FPM	ROLL 1 # OF WRAPS	ROLL 2 # OF WRAPS	ZONE 1 TEMP (C)	ZONE 2 TEMP (C)	ZONE 3 TEMP (C)	ZONE 4 TEMP (C)
CBE-15	30	9.0	11.7	8	12	125	150	190	225
CBE-16	30	9.0	11.7	8	12	125	150	190	225
CBE-16A	30	9.0	11.7	8	12	125	150	190	225
CBE-17	30	9.0	11.7	8	12	125	150	190	225
CBE-18	30	9.0	11.7	8	12	125	150	190	225
CBE-19	30	9.0	11.7	8	12	125	150	190	225

THE HOT-STRETCHED BRAIDS WERE CHARACTERIZED
PER STANDARD SUTURE TEST METHODS:

COMPOSITE BRAID EVALUATION

PHYSICAL PROPERTY CHARACTERIZATION

MGS ID#	USP DIAM (MILS)	ULTIMATE TENSILE STRENGTH (LBS)	INTRINSIC TENSILE STRENGTH (PSI)	INTRINSIC TENSILE STRENGTH (LBS)	INTRINSIC TENSILE STRENGTH (PSI)	KNOT CONVERSION (%)	ULTIMATE ELONGATION (%)	STRAND BENDING RIGIDITY (GMXCM ²)	KNOT STABIL (# THROWS)	BSR CONTROL (LBS)	BSR 21 DAY (LBS)	BSR 21 DAY (%)	PICKS INCH	TOTAL DENIER
CBE-15	18.6	14.14	51758	9.64	35254	68	34	2.24E-2	5	0.00	0.00		44	2529
CBE-16	19.1	13.07	45460	9.52	33116	73	30	2.20E-2	5	0.00	0.00		45	2694
CBE-16A	0.0	0.00	0	0.00	0	0	0	0.00		0.00	0.00		41	2565
CBE-17	19.9	13.88	44850	11.02	35600	79	39	1.28E-2	5	0.00	0.00			
CBE-18	19.5	21.30	71295	13.54	45241	63	27	3.00E-2	4	0.00	0.00			
CBE-19	20.6	7.37	21460	5.96	17763	79	57	1.12E-2	7	0.00	0.00		39	2970

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Experiment No.

Date

2/2/89

Subject

PET/PTFE COMPOSITES

Purpose

CONTINUED:

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DISCUSSION:

FROM A BRAID PROCESSING VIEWPOINT, THE COMMINGLED YARN WAS THE LEAST PROBLEMATIC BRAID FOLLOWED BY THE YARN BLEND. THE CARRIER BLEND PRESENTED THE MOST DIFFICULTIES IN CORE COPPING AND BRAID LOOSENESS. THE COMMINGLED YARN DID POSSESS REGIONS WHERE THE YARNS SEPARATED RESULTING IN BRAIDING DIFFICULTY AND ROUGHNESS.

FROM A PROPERTY VIEWPOINT, THE INTRINSIC TENSILES OF THE THREE COMPOSITES WERE CLOSE AND APPROXIMATED A RULE OF MIXTURES AVERAGE OF THE TWO CONTROL BRAIDS. THE CARRIER BLEND WAS APPROX 10% HIGHER. INTRINSIC KNOT STRENGTHS WERE VERY SIMILAR AMONG THE COMPOSITES AND WERE 75-80% OF THE PET CONTROL KNOT STRENGTH. THE COMM. HAD THE HIGHEST KNOT CONVERSION (72%). THE BENDING RIGIDITY OF THE COMMINGLED WAS HALF THE OTHER TWO COMPOSITES, PERHAPS REFLECTING ITS MORE HOMOGENEOUS MIXTURE OF THE TWO COMPONENTS. ALL 3 COMPOSITES HAD KNOT SECURITIES OF 5 THOUS. SIGNIFICANTLY BETTER THAN 7 FOR 100% PTFE.

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Book No.

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Project No. CBE Experiment No. _____ Date 3/6/89
 Subject VINYL/PDS BRAID COMPOSITE
 Purpose IN-VIVO DATA

BACKGROUND:

THE VINYL/PDS COMPOSITE BRAIDS DESCRIBED
 ON PGS 10-11 WERE TESTED FOR IN-VITRO
 PROPERTIES.

THE FOLLOWING RESULTS WERE OBTAINED BY ERF (89-064):

SAMPLE	SIZE	0-DAY	21 DAY	
		BASELINE (LBS)	(LBS)	(%)
CBE-6	2-0	6.65	2.43	36.5
CBE-7	2-0	9.45	4.07	43.1
CBE-9	2-0	14.51	7.03	48.5
CBE-10	2-0	6.51	1.86	28.6

DISCUSSION

CBE-6 IS A CARRIER BLEND, CBE-7 IS YARN BLEND,
 CBE-9 IS VINYL CONTROL AND CBE-10 IS PDS CONTROL.

THE VINYL CONTROL IS CLOSE TO A PROPER AVERAGE.

THE 2 COMPOSITES FALL BETWEEN THE 2 CONTROLS

AS EXPECTED, HOWEVER THE YARN BLEND RETAINED
 MORE STRENGTH AND WAS STRONGER TO START.

THIS IS POSSIBLY DUE TO DIFFERENCES IN
 EXPOSURE HISTORY.

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Book No.

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Project No. STU Experiment No. _____ Date 4/4/89
 Subject SURFACE TREATMENT VITC
 Purpose IDEA DOCUMENTATION

A SURFACE TREATMENT, SUCH AS PLASMA FLUORINATION WHICH LOWER THE SURFACE ENERGY OF AN ABSORBABLE SURFING, MAY IMPROVE THE SURFING'S BSR DUE TO INHIBITED WETTING OF THE SURFACE BY H_2O . IT IS SPECULATED THAT H_2O MUST FIRST BE ADSORBED ONTO THE POLYMER SURFACE BEFORE HYDROLYSIS (RESULTING IN CHAIN SCLISSON AND STRENGTH DEGRADATION) CAN OCCUR SO THAT SLOWING THE ADSORPTION STEP BY MAKING IT MORE HYDROPHOBIC SHOULD SLOW THE TENSILE LOSS. ADDITIONAL PRODUCT IMPROVEMENTS MAY INCLUDE INCREASED PLIABILITY DUE TO INCREASED FIBER LUBRICITY AS WELL AS IMPROVED KNOT TIE-DOWN.

THE PROCESS WOULD PREFERABLY BE CONTINUOUS. FLUORINE ATOMS WOULD BE GRAFTED ONTO THE POLYMER BACKBONE, THE DEGREE DETERMINED BY THE RESIDENCE TIME AND CONCENTRATION OF THE PLASMA.

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Date 3-15-90

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Book No.

175

Project No.

Experiment No.

Date 5/23/89

Subject

KAWABATA BENDING RIGIDITY CHARACTER

Purpose

EVALUATE ETHIBOND STANDARD - EXTRA, TILAN

BACKGROUND:

THE BENDING RIGIDITY OF SIZE 2-0 ETHIBOND, ETH EXTRA, AND TILAN (0-6) WERE DETERMINED USING THE KAWABATA PUNE BENDING TESTER AT P.C.T. ES. SIX SAMPLES OF EACH WITH 36 STANDARDS PER SAMPLE WERE TESTED (216 TOTAL) AS DESCRIBED ON PG 18.

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RESULTS:

DESCRIP	SUTURE EI (GM-CM ² /STRAND)	STD DEV
ETHIBOND/PRODUCTION/NON-STERIL	3.64 E-2	0.24 E-2
ETHIBOND/PRODUCTION/CO 60	3.64 E-2	0.32 E-2
ETHIBOND EXTRA/NON-STERIL	2.16 E-2	0.22 E-2
TILAN/SILICONE/STERIL*	5.28 E-2	0.42 E-2

* HAND STRETCHED TO MINIMIZE MEMORY

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ANALYSIS

THE DATA SUGGESTS: 1) SIGNIFICANTLY LOWER EI OR "IMPROVED PLIABILITY" FOR ETHIBOND EXTRA, 2) NO SIGNIFICANT EFFECTS OF CO 60 STERIL ON PRODUCTION ETHIBOND EI, AND 3) LOWER EI OR HIGHER PLIABILITY OF CURRENT ETHIBOND VS TILAN. HOWEVER, IT SHOULD BE NOTED THAT THE BRAD M-1C CURVES ARE NON-LINEAR SO THAT THE EI IS DEPENDENT ON WHERE THE SLOPE IS TAKEN. THE ABOVE DATA IS THE TIGHTER REGION OF CURVATURE (K=1.5 TO 2.5 G). IT SHOULD BE NOTED AT LOWER VALUES OF K THAT TILAN IS MORE PLIABLE THAN ETHIBOND STANDARD, BUT THAT ETHIBOND EXTRA EXHIBITS THE LOWEST EI OVER THE ENTIRE RANGE OF CURVATURES.

Investigator

Witness

Date

Date

5/23/89

3-15-90